

A METHOD OF PRODUCING AND IMPROVING AN OPTICAL
TRANSMISSION LINE, AND ASSOCIATED COMPENSATION MODULES

The invention relates to methods of producing and improving an optical transmission line comprising the combination of a line optical fiber and a module for compensating the chromatic dispersion of said line optical fiber. The invention also relates to an original compensation module, i.e. one associated with the line optical fiber from the outset, at the stage of installing the optical transmission line. The invention further relates to a modified compensation module, i.e. modified by the above method of improving the optical transmission line.

In the prior art, a distinction is made between single-band optical transmission lines and multiband optical transmission lines, both of which use, for compensating the chromatic dispersion of the line fiber, modules incorporating one or more chromatic dispersion compensating optical fibers (DCF).

One prior art single-band optical transmission line uses a compensation module comprising an optical fiber for compensating the line optical fiber concerned in the spectral band concerned. A drawback of that prior art is that it is relatively inflexible. If multiband use of an existing optical transmission line is required at a later stage, the compensation module must either be replaced in its entirety or used with other modules in parallel with it.

A prior art single-band optical transmission line described in Patent Application WO01/69822 uses a compensation module within which a plurality of compensating optical fibers of the same type are associated in series, the fibers all providing compensation in the spectral band concerned but differing from one another, for example by virtue of one of them undercompensating in the spectral band concerned while another overcompensates in the same spectral band; thus

the series association of a plurality of compensation optical fibers provides improved compensation in the spectral band concerned, which amounts to widening said spectral band. A drawback of that prior art is that its
5 wideband single-band optical transmission line compensation module is also fixed once installed, and can be replaced only in its entirety.

One prior art multiband optical transmission line uses a plurality of compensation optical fibers in
10 parallel with wavelength division multiplexing and demultiplexing systems. A drawback of that prior art is that it is complex and costly.

A prior art multiband optical transmission line described in paper TuJ6 by Lars Grüner-Nielsen, "Module
15 for simultaneous C+L-band dispersion compensation and Raman amplification", OFC 2002, 19/03/02, uses a module that combines two compensation optical fibers in series. The compensation optical fibers are chosen so that their series combination compensates the chromatic dispersion
20 of the line optical fiber in band C and in band L, but neither of them is optimized for compensation in either band C or band L. That prior art also has the drawback of being fixed once installed.

According to the invention, the original
25 compensation module is based on the use of a plurality of compensation fibers disposed in series to offer compensation that can become multiband compensation on the transmission line concerned. Likewise the modified compensation module offers compensation that is
30 multiband. The invention proposes a method of producing an optical transmission line that is flexible, i.e. for which the number of spectral bands in which the chromatic dispersion compensated can increase without necessitating replacement of the entire compensation module, only a
35 portion of the module. On the optical transmission line, for each new operating spectral band in which chromatic dispersion is to be compensated, it suffices to exchange

one of the submodules of the compensation module; throughout the service life of the optical transmission line there is good compensation of chromatic dispersion over all the spectral bands in which the optical
5 transmission line operates at that time, which guarantees good compensation quality for a lower overall cost. For example, consider a submodule C including an optical fiber providing compensation in band C, of which a length l_0 would be required to compensate a given line optical
10 fiber, and a submodule L including an optical fiber providing compensation in band L, of which a length l_0 would be required to compensate the same line fiber, the two compensation optical fibers being chosen so that their series combination, each with a length of $l_0/2$,
15 offers good compensation in bands C and L. The production method consists of installing the line optical fiber with a compensation module from the outset, which module consists of two independent band C submodules associated in series, which yields an overall length of
20 compensation optical fiber in band C equal to l_0 that is divided into two sublengths $l_0/2$, one per submodule. The optical transmission line operates in band C over a time period of a few years, for example, with very good compensation in band C. After this initial period of
25 operation, the improvement method replaces one of the band C submodules with a band L submodule, the resulting modified compensation module then consisting of the series association of a band C submodule and a band L submodule, the optical transmission line thereafter operating in bands C and L with good compensation in
30 bands C and L. Replacement is easy because the submodules are separable from the structure of the modules and the connections between the submodules are, firstly, identifiable to the naked eye without
35 necessitating optical measurements and, secondly, accessible from outside the module without damaging the module. Over the service life of the optical

transmission line, a shorter length of compensation optical fiber is required, compared to the situation of using an original module optimized for compensation in band C that is later replaced in its entirety by a module
5 optimized for compensation in bands C and L, with a comparable quality of compensation at all times in the service life of the optical transmission line.
Similarly, installing an optical transmission line equipped from the outset with a "modified" compensation
10 module can be envisaged if the optical transmission line is intended to operate in bands C and L, in which case the module consists of three submodules in series, i.e. two band C submodules and one band L submodule, and can evolve afterwards towards a modified compensation module
15 for bands S, C and L, consisting of three submodules in series, i.e. a band S submodule, a band C submodule, and a band L submodule, or a modified compensation module for bands C, L, and U, consisting of three submodules in series, namely a band C submodule, a band L submodule,
20 and a band U submodule.

The invention provides a module for compensating chromatic dispersion of a line optical fiber in a given spectral band, characterized in that the module includes a structure carrying a plurality of submodules at least
25 one of which is separable from the structure, which are disposed in series, which are interconnected by one or more connections identifiable to the naked eye without optical measurement and accessible from the outside without damaging the module, and each of which includes a support to which is fixed at least one optical fiber for
30 compensating chromatic dispersion in said spectral band, said compensation optical fiber being of the same kind for all the submodules. This module is referred to herein as an "original" module.

35 The invention also provides a module for compensating chromatic dispersion of a line optical fiber in a plurality of contiguous and non-overlapping spectral

bands each covering at least 30 nanometers, characterized in that the module includes a structure carrying a plurality of submodules at least one of which is separable from the structure, which are disposed in series, which are interconnected by one or more connections identifiable to the naked eye without optical measurement and accessible from the outside without damaging the module, and each of which includes a support to which is fixed at least one optical fiber for compensating chromatic dispersion, at least one optical fiber of said plurality of compensation optical fibers having a compensation ratio from 0.9 to 1.1 for the center wavelength of one of said spectral bands, at least two submodules having compensation optical fibers of different kinds. This module is referred to herein as a "modified" module.

The invention further provides a method of producing an optical transmission line including a step of installing a line optical fiber and either an original compensation module for said line optical fiber or an existing modified compensation module for said line optical fiber.

The invention further provides a method of improving an optical transmission line comprising a line optical fiber and an existing and previously used original or modified compensation module for said line optical fiber, the method including one or more exchange steps each consisting in removing from said module a submodule and replacing it in said module by a submodule whose compensation optical fiber is of a different kind to the optical fiber of the submodule that has been removed, in order to obtain a modified module.

The invention will be better understood and its other features and advantages will become apparent in the light of the following description and the accompanying drawings, which are provided by way of example, and in which:

- Figure 1 shows diagrammatically one example of an original compensation module of the invention;

- Figure 2 shows diagrammatically one example of a modified compensation module of the invention;

5 - Figure 3 shows diagrammatically the properties of examples of compensation fibers used in compensation modules of the invention;

- Figure 4 shows diagrammatically the structures of examples of compensation fibers used in compensation 10 modules of the invention;

- Figures 5, 7, 9 and 11 show diagrammatically, as a function of wavelength, the cumulative chromatic dispersion over 100 km of an optical transmission line including examples of compensation fibers described with 15 reference to Figures 3 and 4; and

- Figures 6, 8, 10 and 12 show diagrammatically, as a function of wavelength, the chromatic dispersions of examples of compensation fibers described with reference to Figures 3 and 4.

20 The method of the invention of producing an optical transmission line associates an original compensation module of the invention with a line optical fiber. The method of the invention of improving an optical transmission line replaces one of the submodules of an 25 original compensation module of the invention to convert it into a modified compensation module of the invention. A modified compensation module of the invention can also be converted into a compensation module further modified in accordance with the invention by means of the method 30 in accordance with the invention of improving the optical transmission line. Some steps of a method of the invention of producing an optical transmission line can be omitted in order to associate a modified compensation module of the invention with a line optical fiber at the 35 installation stage. In the improvement method of the invention, at least one of the original submodules preferably has neither been nor is subjected to any of

the exchange steps consisting in replacing it with a submodule whose compensation optical fiber is optimized in a spectral band different from its own, but can of course sometimes be replaced by an identical submodule or
5 by a submodule whose compensation optical fiber is optimized in the same spectral band as that corresponding to a "standard" exchange.

The original or modified module of the invention has a structure which carries the submodules. At least one 10 of the submodules can be separated from the structure of the module, and preferably a number of them, namely all the submodules that may have to be replaced, thus enabling them to be replaced individually. Another option is for all the submodules to be separable from the 15 structure of the module. The submodules are preferably independent of one another, i.e. any submodule can be removed from the module without regard to the other submodules. Each submodule has its own support to which the compensation optical fibers that it contains are fixed; it preferably contains only one compensation 20 optical fiber; however, it can contain a plurality, for example in the case of a plurality of line optical fibers in parallel or in a situation where a plurality of optical fibers in series are necessary to provide 25 chromatic dispersion compensation for a spectral band. The compensation optical fiber is fixed to its support, which therefore retains said optical fiber. Each of the submodules preferably has its own casing, i.e. a support that is closed or virtually closed from the outside. The 30 structure of the module can equally be an outer casing containing all the submodule casings or supports.

The submodules are interconnected by one or more connections, each of which can be identified by the naked eye, without optical measurements, and is accessible from 35 outside the module without damaging the module, to facilitate replacement of a submodule with another submodule to improve the optical transmission line. The

connection can be "fixed", for example, such as a weld that is identifiable or rendered identifiable, which has the merit of stability and low degradation of attenuation losses. The connection can also be "demountable", for 5 example, in the manner of a connector, which has the merit of greatly facilitating replacement of a submodule. Other types of "fixed" or "semi-fixed" connection are possible, but should preferably be avoided in that they are not sufficiently stable in time, the transmission 10 line generally being intended to be in service for several years, and at the very least for several months.

The original module comprises a plurality of submodules for compensating chromatic dispersion of a line optical fiber in a given spectral band. Said 15 spectral band is preferably band C, but any other spectral band used by optical transmission lines can be envisaged. The submodules are disposed in series and the optical signal transmitted, on passing through the line optical fiber, therefore passes through the compensation 20 optical fibers of the successive submodules. The submodules are independent of one another, for example, and are interconnected by connections each consisting of a connector or each comprising at least one connector, such as for example the following sequence: connector, 25 component or optical fiber having a particular function, connector, or a plurality of connectors in the case of a transmission line including a plurality of line optical fibers in parallel. The connections can also each consist of a weld or each include at least one weld. 30 Each submodule includes an optical fiber for compensating chromatic dispersion in the spectral band concerned, preferably only one such fiber. The compensation optical fiber is of the same kind for all the submodules, i.e. it is the same fiber having the same compensation ratio in 35 the spectral band concerned, ignoring tolerances and fabrication errors, but different lengths of which may be used from one submodule to another.

The original compensation module preferably includes only two submodules. It can advantageously include three or four submodules. With more than three or four submodules, it becomes more difficult to design the
5 compensation optical fibers so that the replacement of a submodule by another submodule allows the use of an additional spectral band with a good compensation ratio in all the spectral bands used on the optical transmission line.

10 The compensation optical fiber is preferably the same length for all the submodules; using submodules of identical design further reduces costs.

15 The spectral band concerned is preferably band C, i.e. the spectral band extending from a wavelength of approximately 1530 nanometers (nm) to a wavelength of approximately 1570 nm, since this is the spectral band in which line optical fibers have the lowest attenuation and that is given priority, i.e. that is used first when initially installing a single-band optical transmission
20 line intended for multiband operation at a later time.

25 Figure 1 shows diagrammatically one example of an original compensation module of the invention. The module comprises in succession: a line optical fiber 1; a first submodule 4 comprising a compensation optical fiber 2; a connector 6; and a second submodule 5 identical to the submodule 4 and comprising a compensation optical fiber 3 identical to the compensation optical fiber 2. A structure 9 taking the form of an outer casing encloses the above components.

30 The modified module is for compensating chromatic dispersion of a line optical fiber in a plurality of contiguous and non-overlapping spectral bands, for example bands S, C, L and U, although any other spectral band used by line optical fibers can be envisaged. To
35 distinguish single-band optical transmission lines from multiband optical transmission lines, i.e. lines using a plurality of spectral bands in a wider spectral band, a

spectral band is considered to cover at least 30 nm.

The modified compensation module comprises a plurality of submodules in series, so that, on passing through the line optical fiber, the transmitted optical signal passes through the successive compensation optical fibers of the successive submodules. The submodules are independent of one another, for example, and are interconnected by connections each consisting of a connector or each including a connector, for example, as in the following sequence: connector, component or optical fiber having a particular function, connector, or a plurality of connectors in the case of a transmission line comprising a plurality of line optical fibers in parallel. The connections can also each consist of a weld or each include at least one weld. Each submodule includes one, and preferably only one, optical fiber for compensating chromatic dispersion in one of the spectral bands concerned. At least two submodules have compensation optical fibers of different kinds, i.e. have different compensation ratios as a function of wavelength, one being optimized in a given spectral band and the other in another spectral band, for example. A compensation optical fiber is considered optimized in a given spectral band if its compensation ratio for the center wavelength of said spectral band is from 0.9 to 1.1, provided of course that a suitable length is chosen. Each compensation optical fiber preferably has a compensation ratio from 0.9 to 1.1 for the center wavelength of one of the spectral bands. However, it is possible for only one of the compensation optical fibers to be optimized for one of the spectral bands, for example the compensation optical fiber contained in the submodules of the original module. In the case of a modified module compensating in bands C and L and comprising two submodules, for example, the first submodule having a compensation optical fiber optimized in band C, the second submodule preferably, but not

necessarily, has a compensation optical fiber optimized in band L, and said optical fiber need not be optimized in any spectral band (this is the case of Example 3, for the fiber designated DCF 3, as shown in Figures 3 and 4
5 and described below); nevertheless, its series combination with the compensation optical fiber of the first submodule must nevertheless offer good compensation in bands C and L.

The modified compensation module preferably
10 comprises only two submodules. It can advantageously also include three or four submodules. With more than three or four submodules, it becomes more difficult to design compensation optical fibers so that the replacement of one submodule by another submodule allows
15 the use of an additional spectral band with a good compensation ratio in all the spectral bands used on the optical transmission line.

The compensation optical fiber is preferably the same length for all the submodules; using submodules of
20 identical design further reduces costs.

The spectral bands concerned are preferably bands C and L, i.e. the spectral bands from a wavelength of approximately 1530 nm to a wavelength of approximately 1570 nm for band C and from a wavelength of approximately 1570 nm to a wavelength of approximately 1610 nm for band
25 L.

Figure 2 shows diagrammatically one example of a modified compensation module of the invention. The module comprises in succession: a line optical fiber 1; a
30 first submodule 4 comprising a compensation optical fiber 2; a connector 6; and a second submodule 8 different from the submodule 4 and comprising a compensation optical fiber 7 different from the compensation optical fiber 2, the compensation optical fibers 2 and 7 being optimized in respective different contiguous and non-overlapping spectral bands, the wavelength of 1570 nm forming the boundary between them. A structure 9 in the form of an
35

outer casing encloses the above components.

In the case of a two-band optical transmission fiber, the modified compensation module comprises two submodules in series connected by a connector, for example. A first spectral band B1 has a center wavelength λ_1 and a contiguous and non-overlapping second spectral band B2 has a center wavelength λ_2 . A preferred method of determining the trend of the chromatic dispersion of each of the two compensation optical fibers in each of the two spectral bands is described below.

Let L, L_1 , L_2 respectively be the length of the line optical fiber, the length of the first compensation optical fiber F1 in the first spectral band B1, and the length of the second compensation optical fiber F2 in the second spectral band B2. Let $C(\lambda)$, $C_1(\lambda_1)$, $C_2(\lambda_2)$ be the respective chromatic dispersions of the line optical fiber, the first compensation optical fiber F1 in the first spectral band B1, and the second compensation optical fiber F2 in the second spectral band B2.

For a given application, let M be the maximum cumulative chromatic dispersion that is acceptable for the optical transmission line, consisting of the line optical fiber, the first compensation optical fiber F1, and the second compensation optical fiber F2, at the respective center wavelengths λ_1 and λ_2 of the spectral bands B1 and B2. The following conditions, in which M is preferably from 0 to 50 ps/nm, therefore apply at these two center wavelengths:

$$|LC(\lambda_1) + L_1C_1(\lambda_1) + L_2C_2(\lambda_1)| \leq M \quad (1)$$

$$|LC(\lambda_2) + L_1C_1(\lambda_2) + L_2C_2(\lambda_2)| \leq M \quad (1)$$

Let N_1 be the cumulative chromatic dispersion at the center wavelength λ_1 of the spectral band B1 for the optical transmission line if the compensation module were to comprise two identical submodules each incorporating a compensation fiber F1. The following condition would then apply at the center wavelength λ_1 :

$$LC(\lambda_1) + 2L_1C_1(\lambda_1) = N_1 \quad (2)$$

Let N_2 be the cumulative chromatic dispersion at the center wavelength λ_2 of the spectral band B2 for the optical transmission line if the compensation module were to comprise two identical submodules each incorporating a 5 compensation fiber F2. The following condition would then apply at the center wavelength λ_2 :

$$LC(\lambda_2) + 2L_2C_2(\lambda_2) = N_2 \quad (3)$$

The values of N_1 and N_2 are preferably made equal, and range from 0 to 50 ps/nm, so that the combination of 10 the two identical submodules offers good chromatic dispersion compensation in a spectral band.

Consider limited developments of the chromatic dispersions of the fibers F1 and F2 in the following form:

$$C_1(\lambda) = a_1 + b_1(\lambda - \lambda_1) + c_1/2(\lambda - \lambda_1)^2 + o(\lambda^3) \quad (4)$$

$$C_2(\lambda) = a_2 + b_2(\lambda - \lambda_2) + c_2/2(\lambda - \lambda_2)^2 + o(\lambda^3) \quad (4)$$

For optical fibers for which the terms of third or higher order would not be negligible, the usual numerical methods remain applicable. These numerical methods 20 enable the conditions (1) to be satisfied for a greater number of wavelengths.

The coefficients a_1 and a_2 are determined from equations (2) and (3).

Let τ_1 and τ_2 be the compensation ratios of the 25 fibers F1 and F2, respectively, with values ranging from 0.9 to 1.1, for the combination of two identical submodules offering good chromatic dispersion compensation ratios in a spectral band, said compensation ratios being defined by the following equations, in which 30 C' is the chromatic dispersion slope of the line optical fiber:

$$\frac{b_1}{a_1} = \tau_1 \left(\frac{C'(\lambda_1)}{C(\lambda_1)} \right) \quad (5)$$

$$\frac{b_2}{a_2} = \tau_2 \left(\frac{C'(\lambda_2)}{C(\lambda_2)} \right) \quad (5)$$

Once the coefficients a_1 and a_2 have been determined

from equations (2) and (3), the coefficients b_1 and b_2 can be determined from equations (5).

Substituting equations (4) in equations (1), and using equations (2) and (3), we obtain:

$$5 \quad C_{1m} \leq c_1 \leq 0 \quad (6)$$

$$C_{2m} \leq c_2 \leq 0 \quad (6)$$

in which:

$$c_{1m} = -\frac{2a_1}{\Delta^2 f_1} \left(-2M + 2N_1 - f_2 + f_1 + \frac{b_1}{a_1} \Delta f_1 \right)$$

$$c_{2m} = -\frac{2a_2}{\Delta^2 f_2} \left(-2M + 2N_2 - f_1 + f_2 - \frac{b_2}{a_2} \Delta f_2 \right)$$

$$10 \quad f_i = LC(\lambda_i) - N_i \quad (i = 1, 2); \quad \Delta = \lambda_2 - \lambda_1$$

Conditions (6) must be satisfied by the coefficients c_1 and c_2 of the fibers F1 and F2.

Figure 3 shows diagrammatically the properties of examples of compensation fibers used in compensation modules of the invention. Figure 3 takes the form of a table with nine columns and eight rows. The first row specifies properties of the chromatic dispersion compensation optical fibers. The next seven rows correspond to seven examples of compensation optical fibers. The first column gives the numbers of the examples. The second column gives the ratio, expressed in nm, between the chromatic dispersion and the chromatic dispersion slope at a wavelength of 1550 nm. The third column gives the type of compensation optical fiber, DCF band C indicating a compensation optical fiber optimized in band C, DCF band L indicating a compensation optical fiber optimized in band L, and DCF 3 indicating a compensation optical fiber that is not optimized either in band C or in band L. The fourth column gives the length in kilometers (km) of compensation optical fiber used in the corresponding submodule, when the length of the line optical fiber is 100 km. The fifth column gives the chromatic dispersion in ps/(nm.km) at the wavelength of 1550 nm. The sixth column gives the chromatic

dispersion slope in ps/(nm².km) at the wavelength of 1550 nm. The seventh and last column gives the effective surface area in μm² at a wavelength of 1550 nm.

Figure 4 shows diagrammatically the structures of examples of compensation fibers used in the compensation modules of the invention. Figure 4 takes the form of a table comprising seven columns and eight rows. The first row gives the names of the structural elements of the chromatic dispersion compensation optical fibers. The next seven rows correspond to seven examples of compensation optical fibers. The first column gives the numbers of the examples. The next three columns give the outside radii of three respective slices constituting the core (in the wide sense, i.e. the variable portion of the index profile extending from the center to the constant index exterior cladding) of each of the compensation optical fibers, expressed in micrometers (μm). The last three columns respectively give 1000 times the index differences between, firstly, the three slices constituting the core (in the wide sense, i.e. the variable portion of the index profile extending from the center to the constant index exterior cladding) of each of the compensation optical fibers and, secondly, the constant index exterior cladding of said compensation optical fibers. All the compensation optical fibers considered correspond to an index profile including a core (in the narrow sense, i.e. the central section of the profile conveying most of the energy), a buried interior cladding and a ring.

Figures 5, 7, 9 and 11 show diagrammatically, as a function of wavelength, the cumulative chromatic dispersion on a transmission line including examples of compensation fibers as described with reference to Figures 3 and 4. The cumulative chromatic dispersion in ps/nm for the whole of the optical transmission line including the line fiber and the two compensation optical fibers connected in series is plotted on the ordinate

axis. The wavelength in nm is plotted on the abscissa axis. Each curve indicates, as a function of wavelength, the cumulative chromatic dispersion of an optical transmission line consisting of the line optical fiber, a 5 first submodule comprising a compensation optical fiber, and a second submodule comprising a compensation optical fiber, these components being disposed in series.

Consider Figure 5. For the curve A, the first submodule incorporates a compensation optical fiber 10 corresponding to Example 1 and the second submodule incorporates a compensation optical fiber also corresponding to Example 1. For the curve B, the first submodule incorporates a compensation optical fiber corresponding to Example 2 and the second submodule 15 incorporates a compensation optical fiber also corresponding to Example 2. For the curve C, the first submodule incorporates a compensation optical fiber corresponding to Example 1 and the second submodule incorporates a compensation optical fiber corresponding 20 to Example 2.

Consider Figure 7. For the curve A, the first submodule incorporates a compensation optical fiber corresponding to Example 1 and the second submodule incorporates a compensation optical fiber also 25 corresponding to Example 1. For the curve B, the first submodule incorporates a compensation optical fiber corresponding to Example 3 and the second submodule incorporates a compensation optical fiber also corresponding to Example 3. For the curve C, the first 30 submodule incorporates a compensation optical fiber corresponding to Example 1 and the second submodule incorporates a compensation optical fiber corresponding to Example 3.

Consider Figure 9. For the curve A, the first 35 submodule incorporates a compensation optical fiber corresponding to Example 4 and the second submodule incorporates a compensation optical fiber also

corresponding to Example 4. For the curve B, the first submodule incorporates a compensation optical fiber corresponding to Example 5 and the second submodule incorporates a compensation optical fiber also
5 corresponding to Example 5. For the curve C, the first submodule incorporates a compensation optical fiber corresponding to Example 4 and the second submodule incorporates a compensation optical fiber corresponding to Example 5.

10 Consider Figure 11. For the curve A, the first submodule incorporates a compensation optical fiber corresponding to Example 6 and the second submodule incorporates a compensation optical fiber also corresponding to Example 6. For the curve B, the first
15 submodule incorporates a compensation optical fiber corresponding to Example 7 and the second submodule incorporates a compensation optical fiber also corresponding to Example 7. For the curve C, the first submodule incorporates a compensation optical fiber corresponding to Example 6 and the second submodule
20 incorporates a compensation optical fiber corresponding to Example 7.

In all of Figures 5, 7, 9 and 11, the curves A show that single-band compensation in band C is good and the
25 curves C show that two-band compensation in bands C and L is also good.

Figures 6, 8, 10 and 12 show diagrammatically as a function of wavelength the chromatic dispersions of examples of compensation fibers as described with
30 reference to Figures 3 and 4.

The chromatic dispersion in ps/nm.km for the compensation optical fiber concerned is plotted on the ordinate axis. The wavelength in nm is plotted on the abscissa axis.

35 In Figure 6, curve D corresponds to the compensation fiber of Example 1 and curve E corresponds to the compensation fiber of Example 2.

In Figure 8, curve D corresponds to the compensation fiber of Example 1 and curve E corresponds to the compensation fiber of Example 3.

5 In Figure 10, curve D corresponds to the compensation optical fiber of Example 4 and curve E corresponds to the compensation fiber of Example 5.

In Figure 12, curve D corresponds to the compensation fiber of Example 6 and curve E corresponds to the compensation fiber of Example 7.